

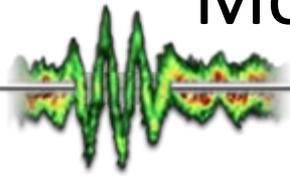
# The Petawatt Field Synthesizer – towards high energy few-cycle pulses

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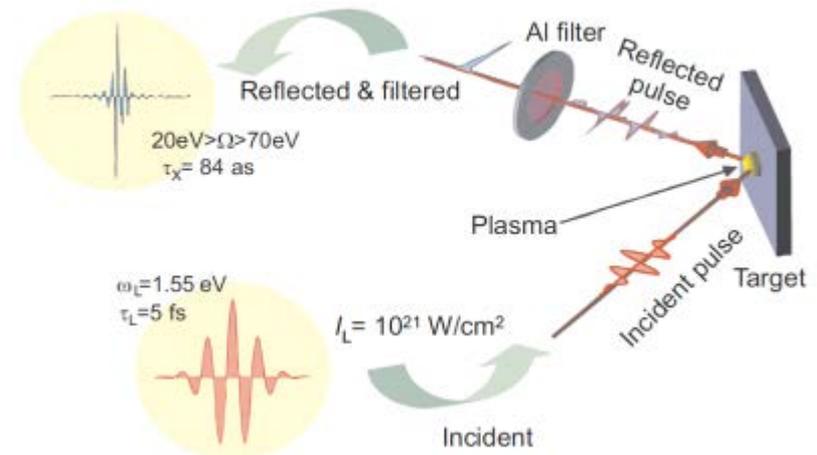
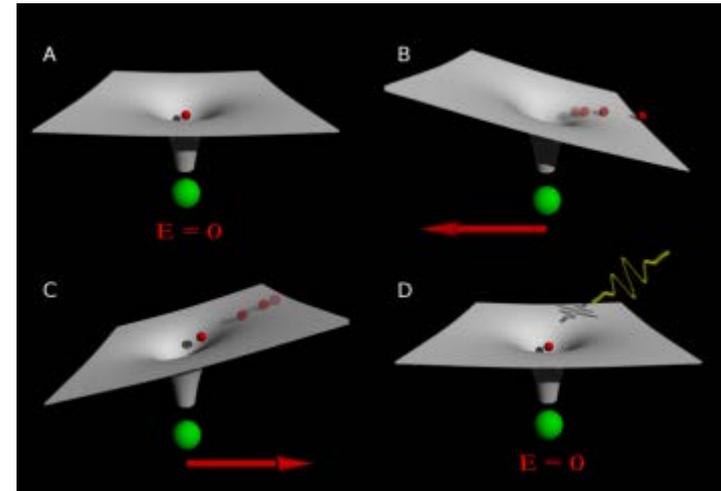
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Germany

# Motivation: Single attosecond pulse generation



## HHG in gas:

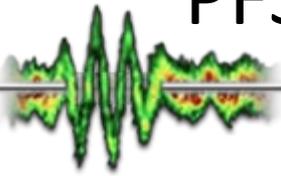
- Low efficiency
- Not scalable in laser intensity



## HHG from solid surfaces:

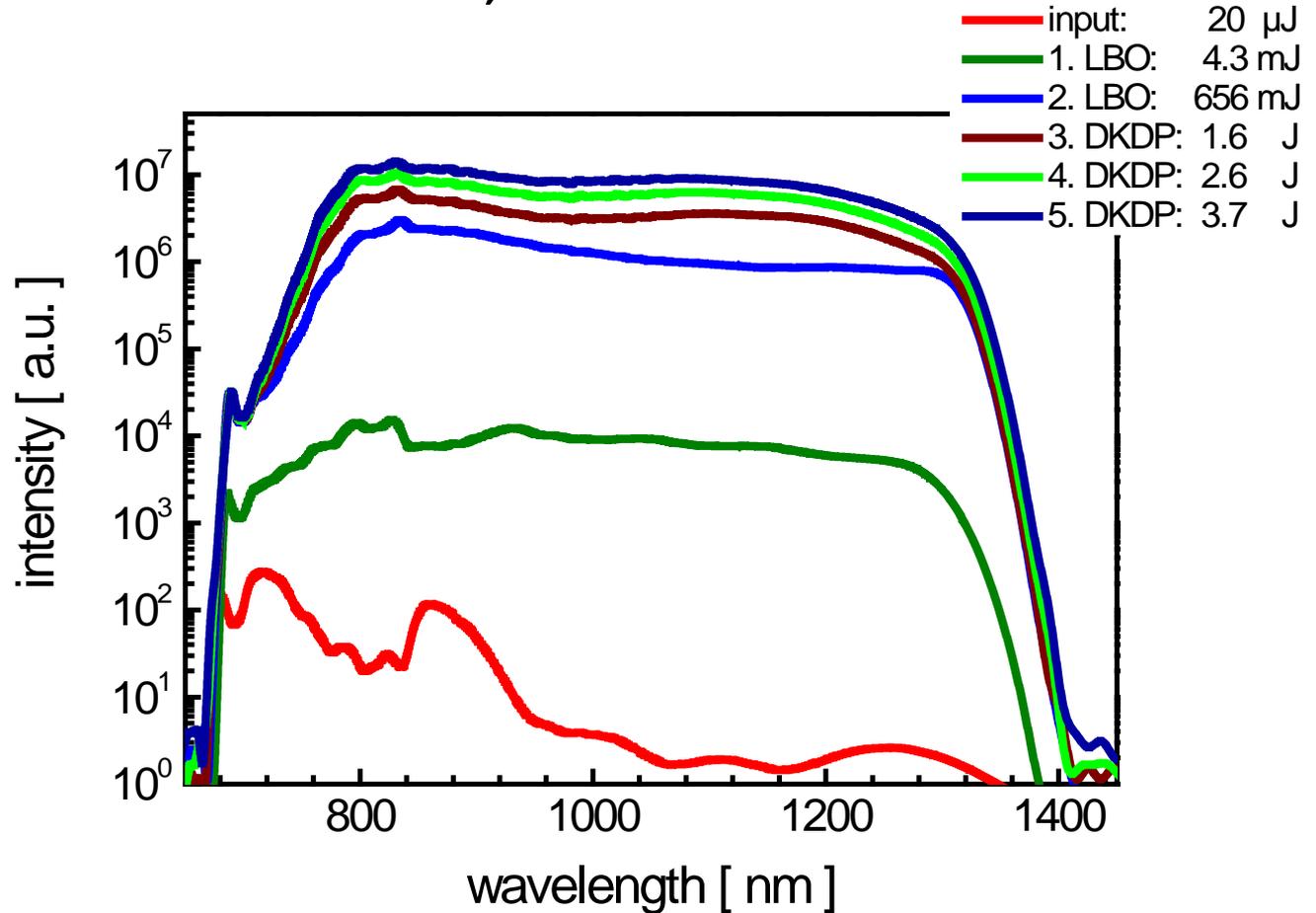
- higher efficiency
- Wavelength and photon flux scales with laser intensity
- **For single attosecond pulse: relativistic, CEP-stable few-cycle pulses needed**

# PFS design considerations



5 fs  $\rightarrow$  broad band  
 $\rightarrow$  High intensity

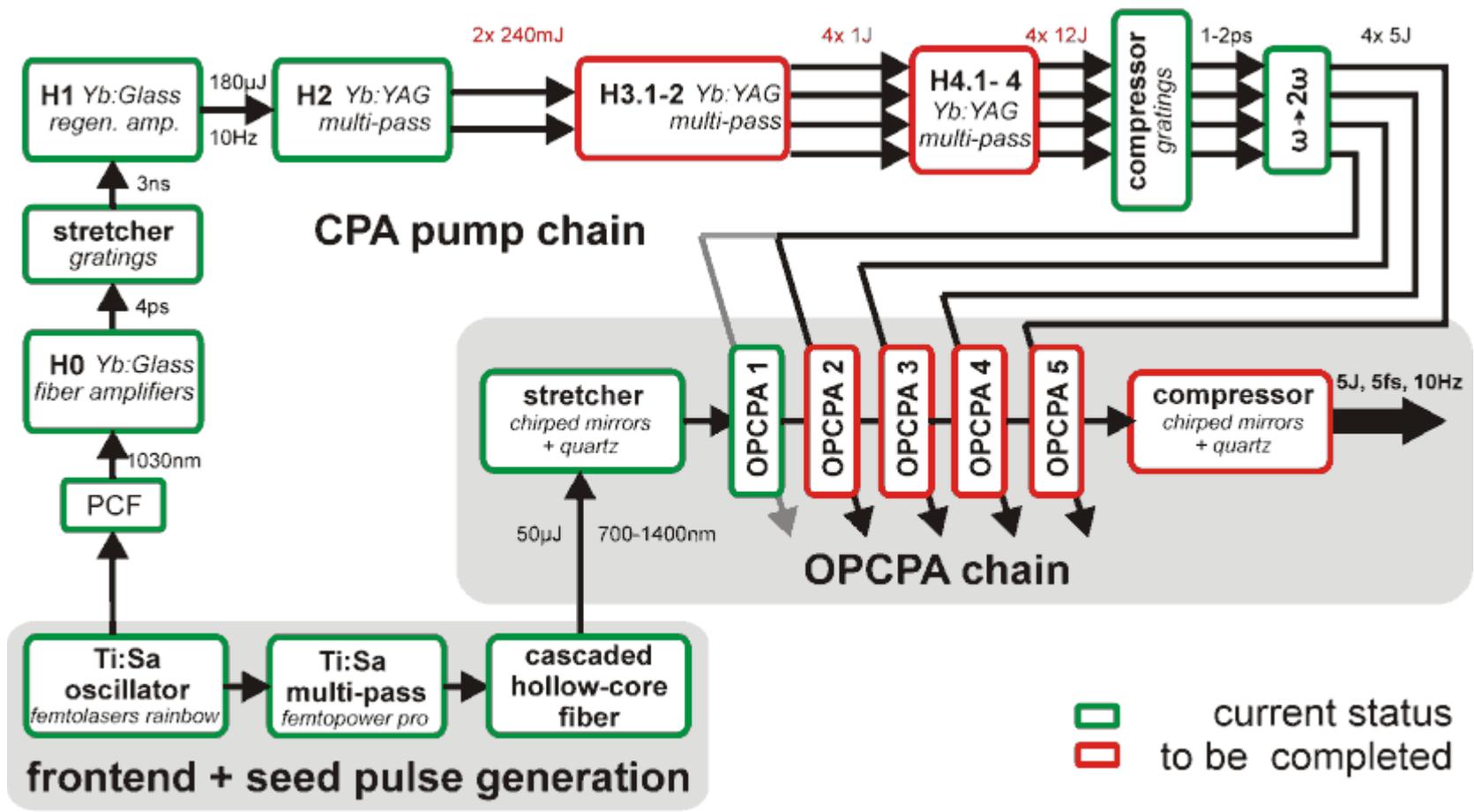
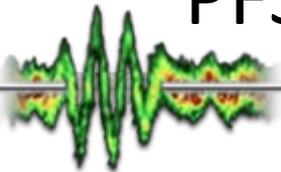
Goal: 5 fs, few J



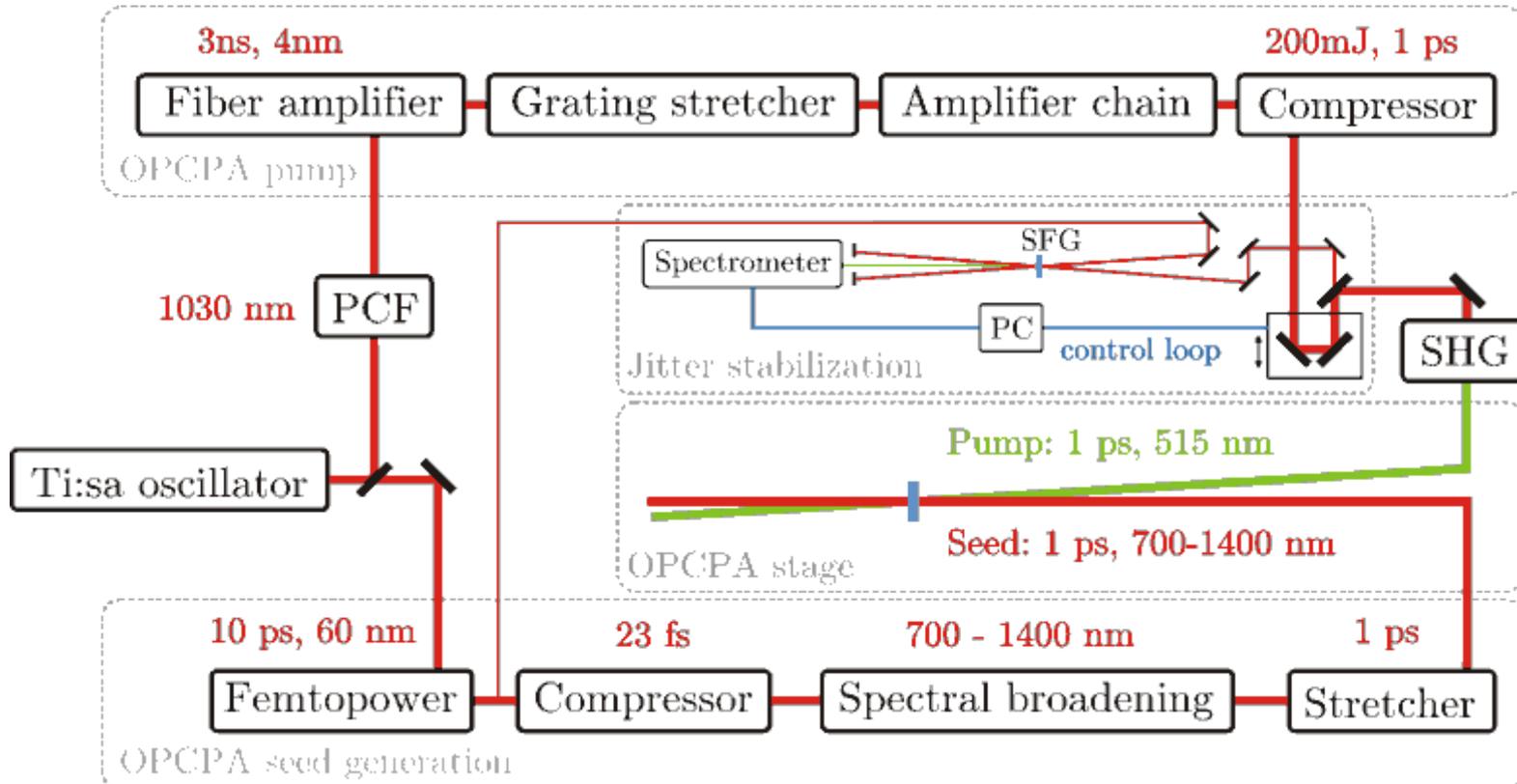
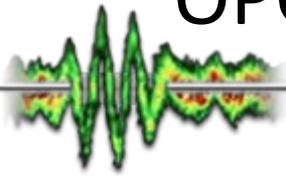
The main challenges :

- seed generation
- pump laser development (4x 5J, 1ps @ 515 nm)
- Pump-seed synchronization

# PFS Layout

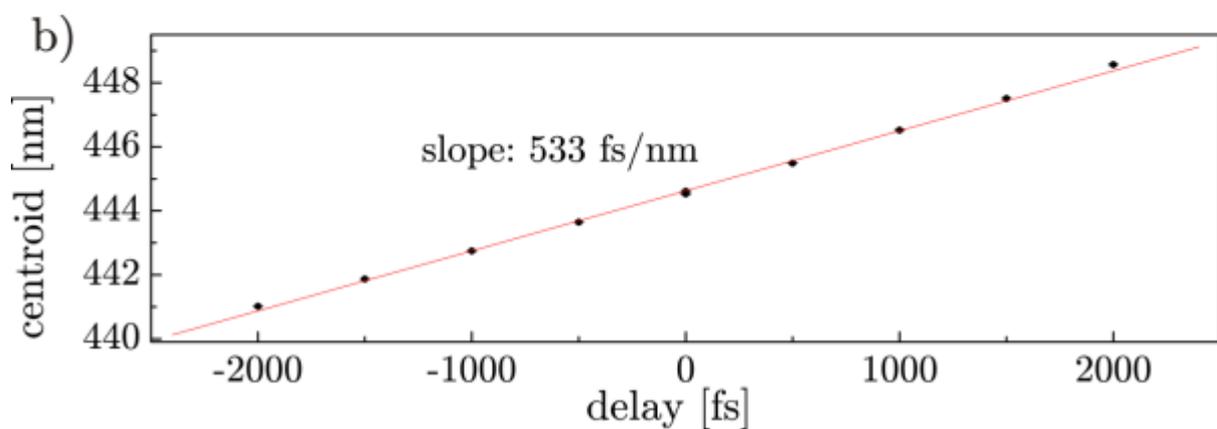
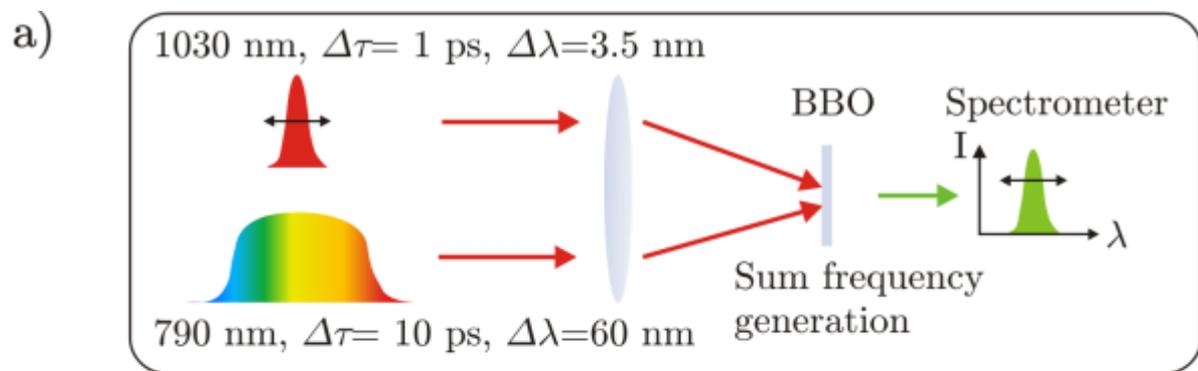
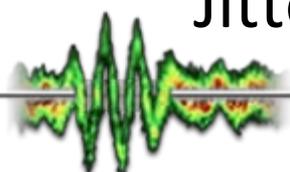


# OPCPA + timing jitter

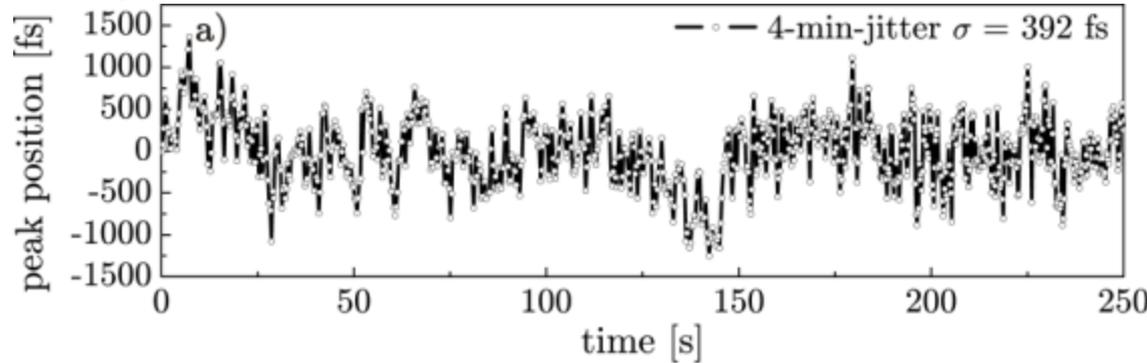
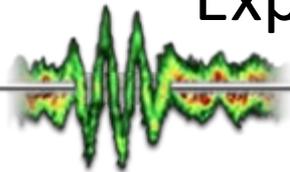


Before first OPCPA- resolve jitter problem!

# Jitter measurement



# Experimental investigation of timing jitter

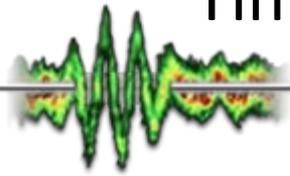


Full pump chain

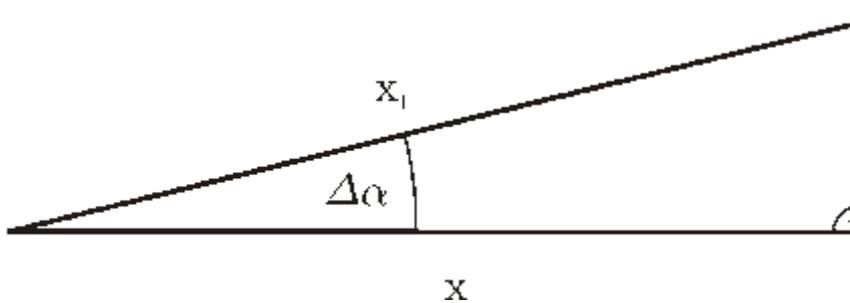
Optical path inside stretcher/compressor has larger effect on timing jitter compared to free space propagation

Can air fluctuations inside stretcher/compressor cause large timing jitter?  
→ Check influence of angle deviations on timing

# Timing jitter from angle deviation



Can shot-to-shot pointing fluctuation (few  $\mu\text{rad}$ ) cause timing jitter?



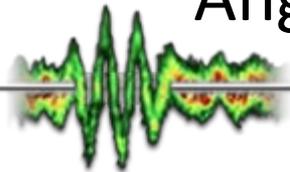
$$x - x_1 = x \left( 1 - \frac{1}{\cos(\Delta\alpha)} \right) \\ \approx \frac{x \cdot \Delta\alpha^2}{2}$$

Example:  $x=100\text{m}$ ,  $\Delta\alpha=10\mu\text{rad} \rightarrow \Delta x= 50\text{nm} \rightarrow \Delta\tau =0.17\text{fs}$

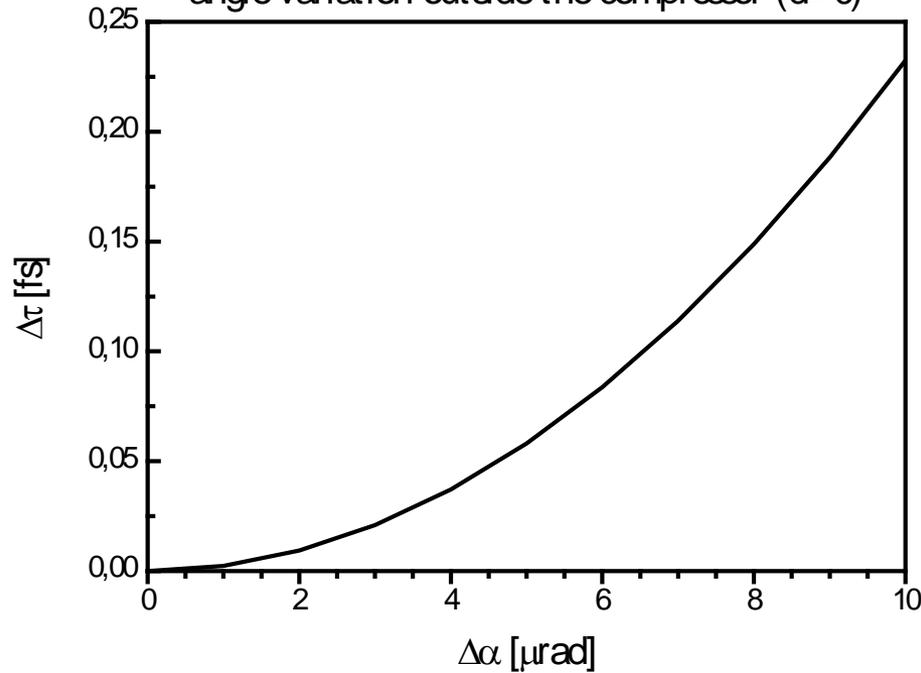
This effect is negligible in most cases!



# Angle fluctuation outside compressor (d=0)



angle variation outside the compressor (d=0)

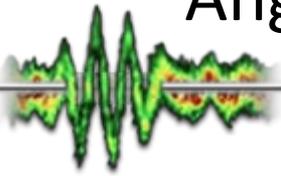


- $N = 1740$  lines/mm
- $\lambda_0 = 1030$  nm
- $\alpha_0 = 58.5^\circ$
- $\beta_0 = 69.97^\circ$
- $L_1 = 6$  m
- $L_2 = 3$  m

$$\Delta\tau = \frac{L_1}{c} \left( \frac{\Delta\beta_2 N \lambda_0}{\cos(\beta_0 - \Delta\beta_2)} - \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 + \Delta\beta_1)} \right)$$

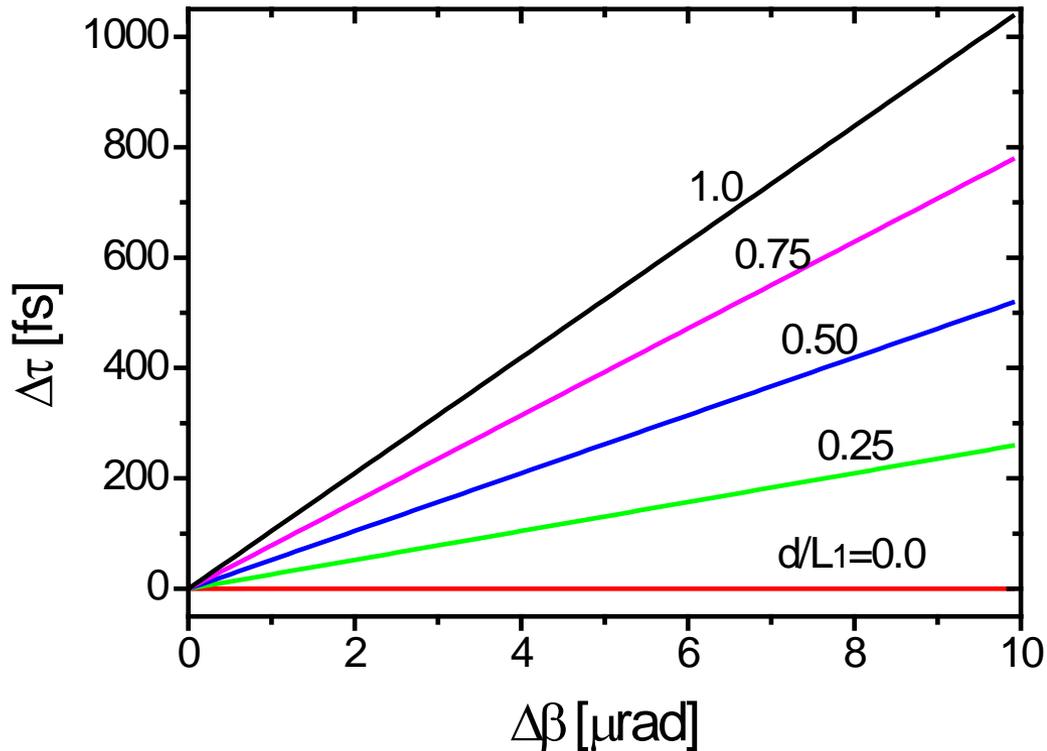
Pathdifference from path to the endmirror  
 And back from endmirror cancel out nearly

# Angle fluctuation inside the compressor



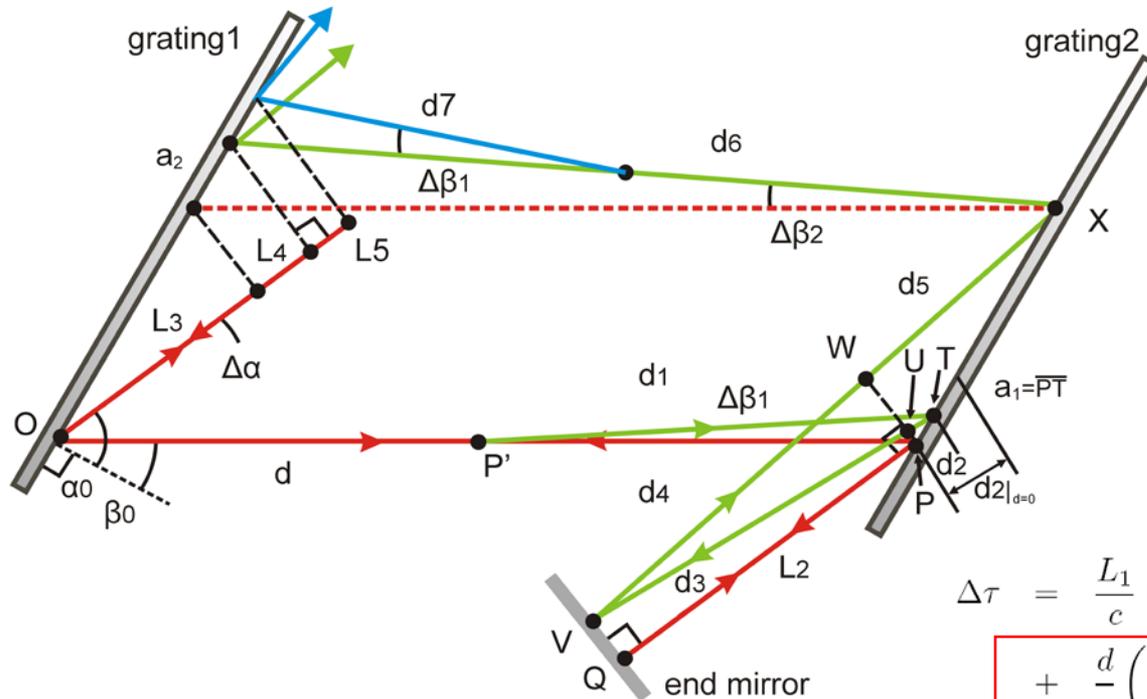
$$\Delta\tau = \frac{L_1}{c} \left( \frac{\Delta\beta_2 N \lambda_0}{\cos(\beta_0 - \Delta\beta_2)} - \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 + \Delta\beta_1)} \right) + \frac{d}{c} \left( \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 + \Delta\beta_1)} \right)$$

→ significantly increased timing jitter



# Still not the truth!

Perturbance will also be there on the backpropagation:



new terms:

$$d_6 = (L_1 - d) \frac{\cos(\beta_0)}{\cos(\beta_0 - \Delta\beta_2)}$$

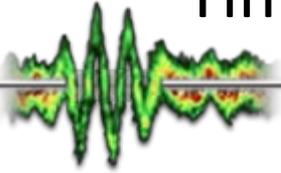
$$d_7 = d \frac{\cos(\beta_0 - \Delta\beta_2)}{\cos(\beta_0 - \Delta\beta_1 - \Delta\beta_2)}$$

$$L_5 = d \frac{\sin(\Delta\beta_1)}{\cos(\beta_0 - \Delta\beta_1 - \Delta\beta_2)} \sin(\alpha_0)$$

$$\Delta\tau = \frac{L_1}{c} \left( \frac{\Delta\beta_2 N \lambda_0}{\cos(\beta_0 - \Delta\beta_2)} \right) - \frac{(L_1 - d)}{c} \left( \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 + \Delta\beta_1)} \right) + \frac{d}{c} \left( \frac{\cos(\beta_0)}{\cos(\beta_0 - \Delta\beta_2)} - 1 + \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 - \Delta\beta_1 - \Delta\beta_2)} \right)$$

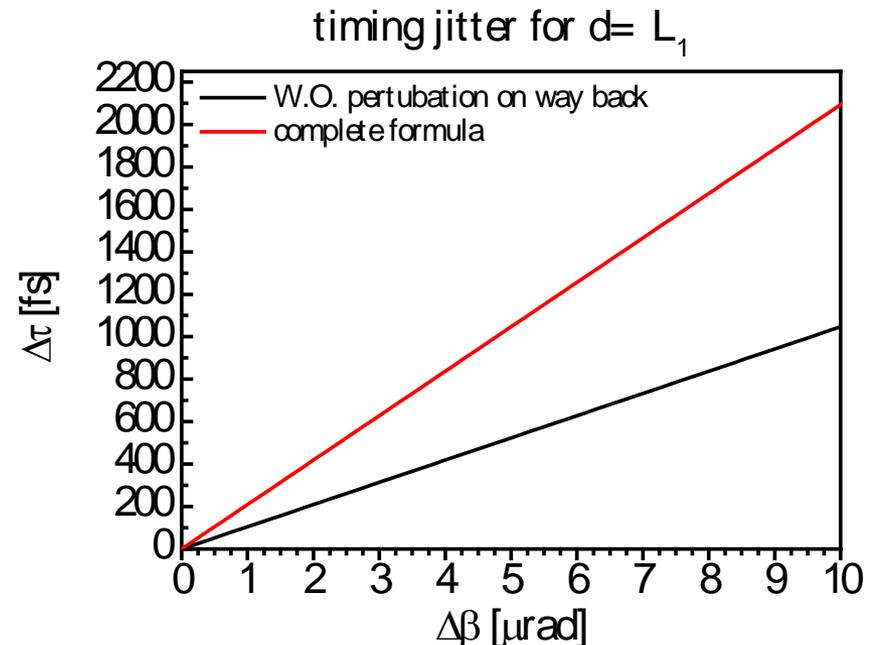
$$\Delta\tau = \frac{d}{c} \left( \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 + \Delta\beta_1)} + \frac{\cos(\beta_0)}{\cos(\beta_0 - \Delta\beta_2)} - 1 + \frac{\Delta\beta_1 N \lambda_0}{\cos(\beta_0 - \Delta\beta_1 - \Delta\beta_2)} \right) \rightarrow \text{approximately doubles jitter}$$

# Timing jitter

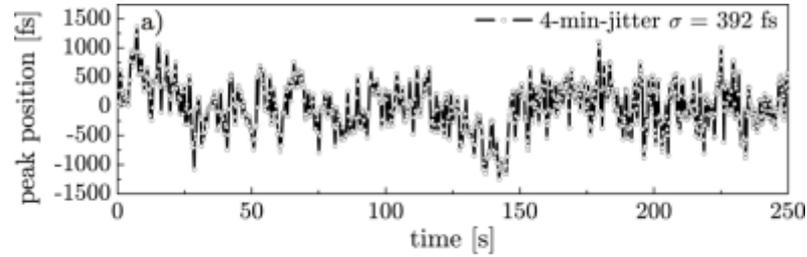
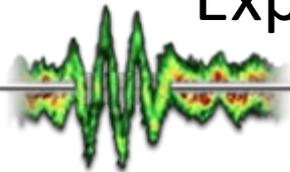


- From experiment we suspect the stretcher/compressor to cause main timing jitter
- beam pointing outside the compressor has negligible effect
- beam pointing inside the compressor can introduce significant timing jitter
- Angle perturbation could arise from air turbulence or mechanical stability of optical components
- results account also for stretcher

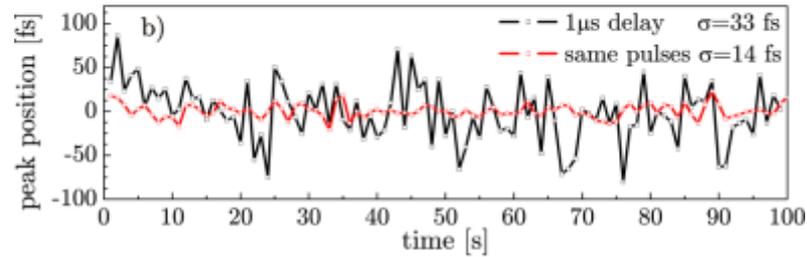
$$\Delta\tau \approx \frac{2 N \lambda_0}{c \cdot \cos(\beta_0)} \Delta\beta_1 d$$



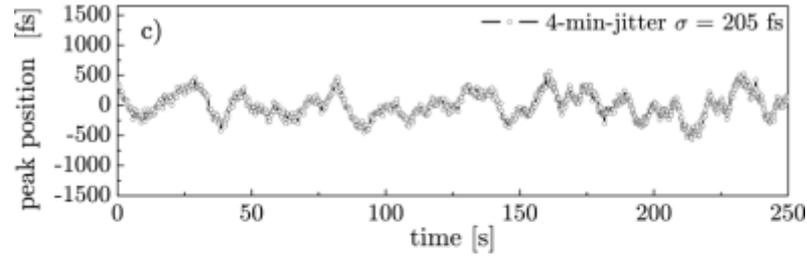
# Experimental investigation of timing jitter



Full pump chain



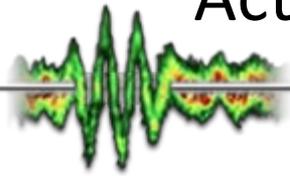
Regen without stretcher/compressor



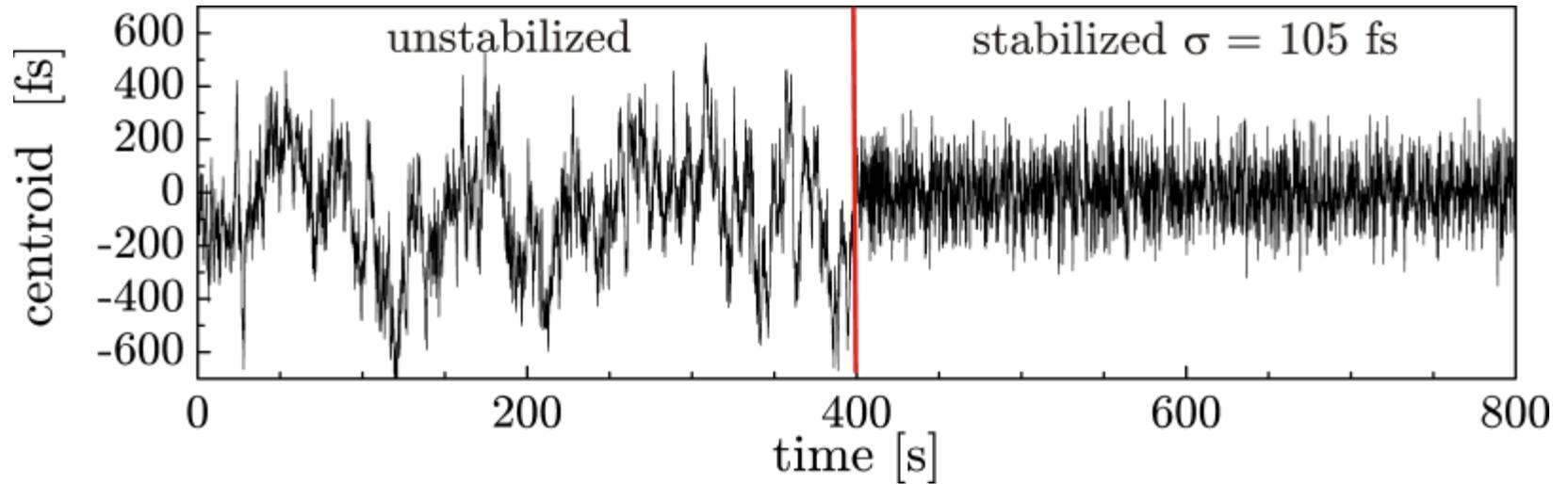
Full pump chain – reduced air turbulence

Air-tight housing for stretcher and beam tubes in the compressor reduce air turbulence and timing jitter.

# Active stabilization

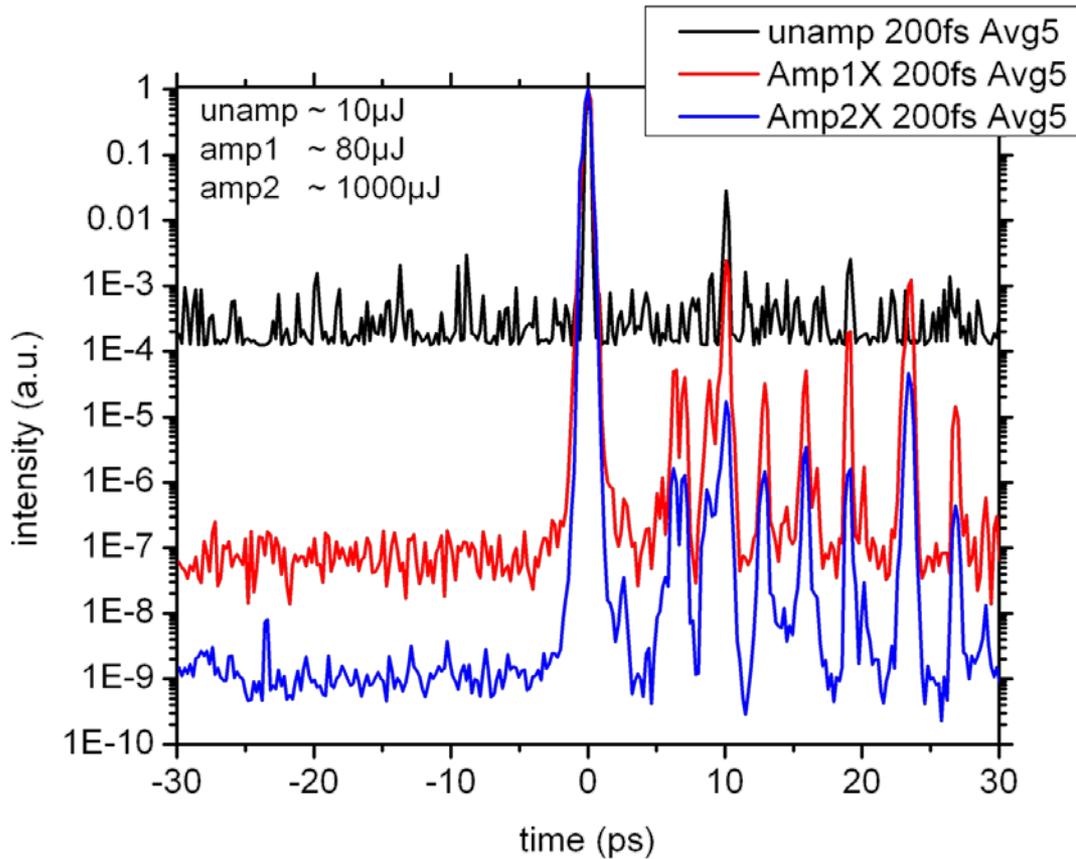


- Move a delaystage according to measured jitter
- works with 10 Hz (on every shot)

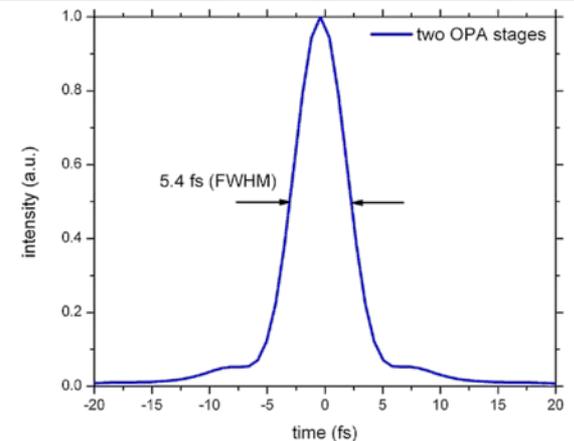


# Preliminary OPCPA results

4 mm & 2 mm LBO and a pump energy of 50 mJ,  $E_{\text{out}} = 3\text{mJ}$

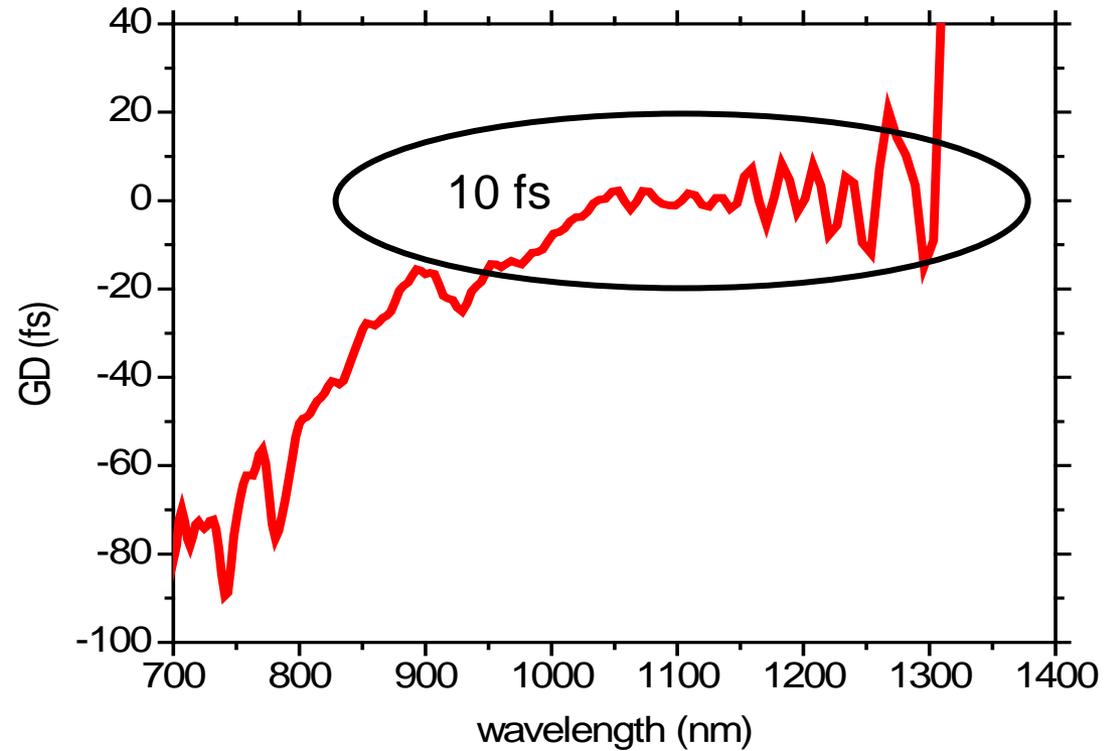
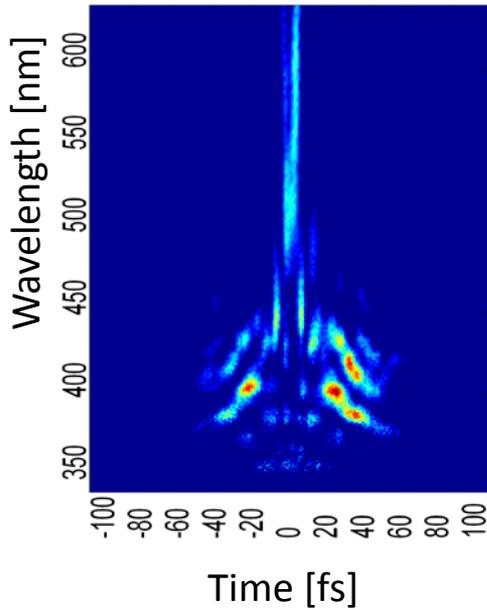


Fourier limit

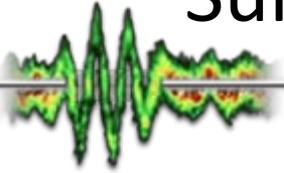


# Preliminary OPCPA results

First compression with CaF + chirped mirrors

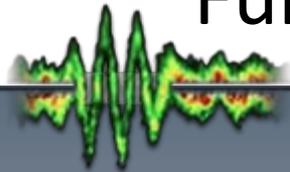


# Summary

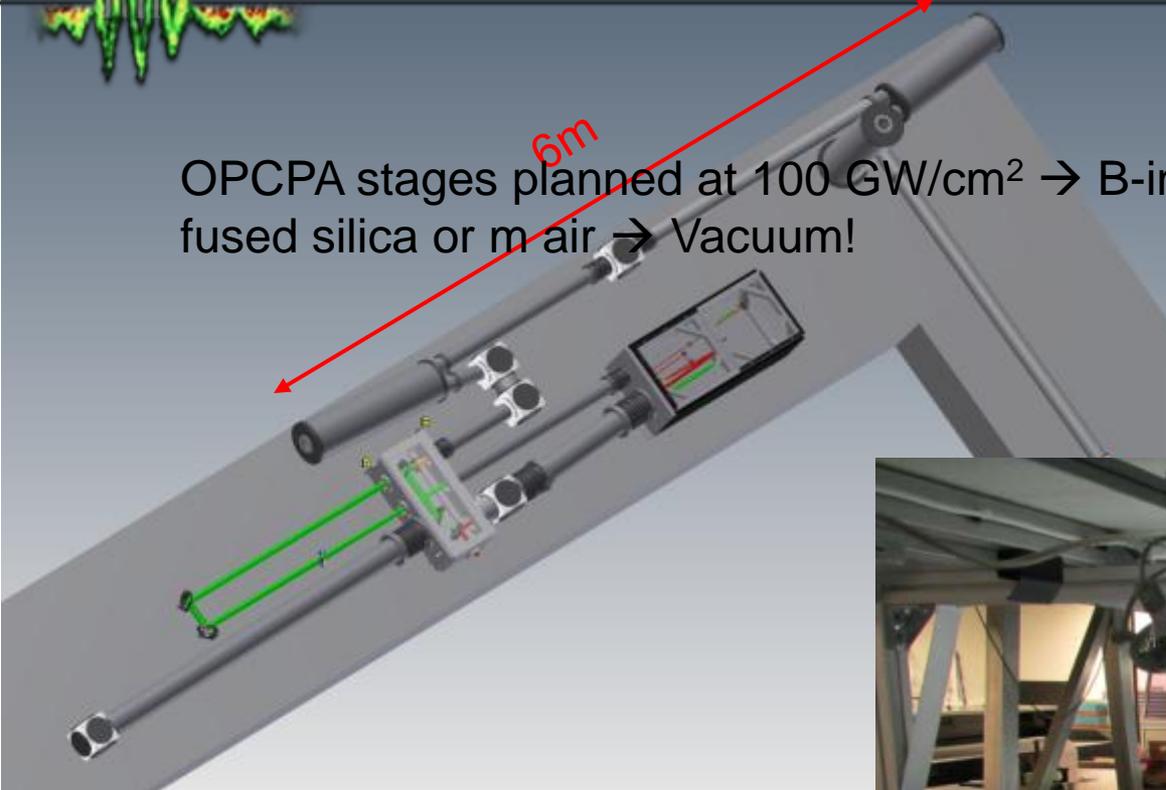


- Timing jitter between seed and pump is investigated experimentally
- it is shown theoretically, that the main source are angular deviations inside the stretcher/compressor
- The jitter could be reduced to 100 fs std by reduced air turbulences and an active stabilization
- First OPCPA results are promising: bandwidth, contrast & compression

# Further steps

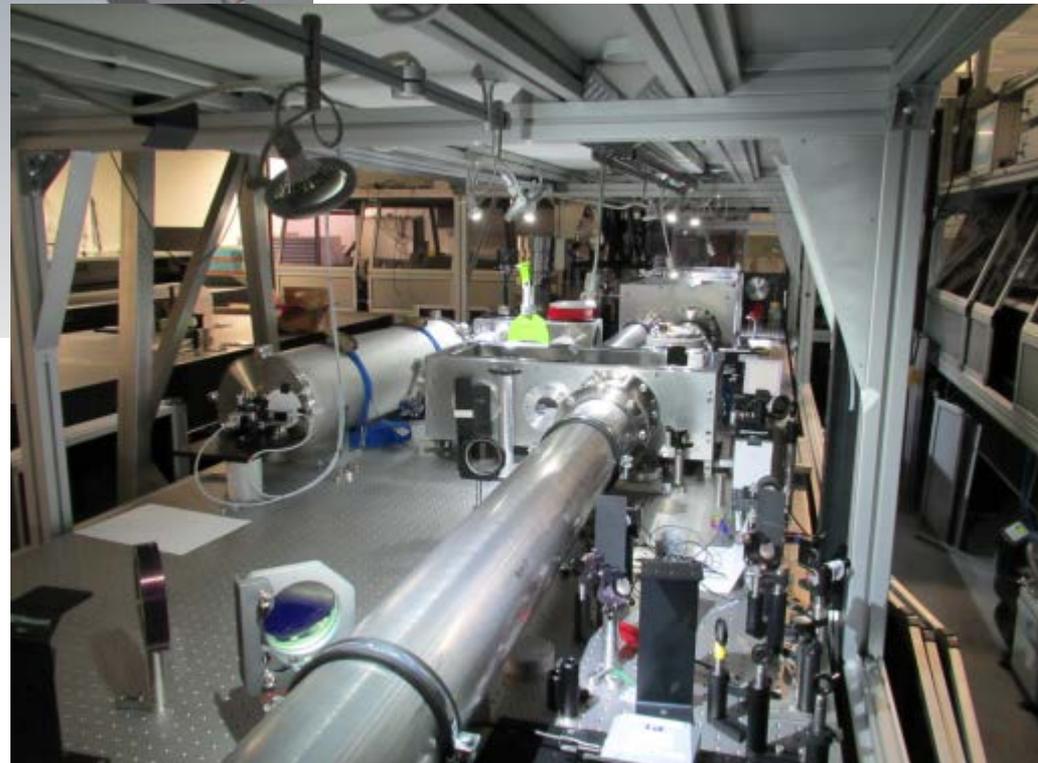


OPCPA stages planned at  $100 \text{ GW/cm}^2 \rightarrow$  B-integral  $B=0.36$  per mm  
fused silica or m air  $\rightarrow$  Vacuum!

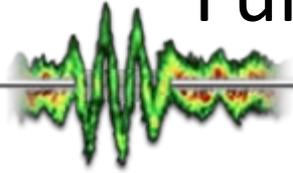


Can use up to 1J (0.5J) pump beam  
in 2 OPCPA stages

For 10 J (5J) pump beam:  
Compressor chamber needed



# Further steps



- Implementation of the high energy pump laser stages
- See Christophs talk on Friday

**Thank you for your attention!**